

Rosconn Strategic Land

Land South of Radwinter Road (East of Griffin Place), Saffron Walden

Flood Risk Assessment

July 2021



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Prepared by **COTSWOLD** TRANSPORT PLANNING LTD CTP House Knapp Road

Cheltenham

Gloucestershire

GL50 3QQ

Tel: 01242 523696 Email: <u>cheltenham@cotswoldtp.co.uk</u> Web: <u>www.cotswoldtp.co.uk</u>



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1 Introduction

Background

- 1.1 Cotswold Transport Planning has been appointed by Rosconn Strategic Land (herein referred to as "the Applicant") to produce a Flood Risk Assessment (FRA) for an outline residential proposal of up to 233 dwellings on Land South of Radwinter Road (East of Griffin Place), Saffron Walden.
- 1.2 The purpose of this FRA is to assess the risk of flooding to the proposed development and where possible provide sufficient mitigation to demonstrate that the future users of the development would remain safe throughout its lifetime, that the development would not increase flood risk on site and elsewhere and, where practicable, that the development would reduce flood risk overall.

National & Local Policies

- 1.3 The National Planning Policy Framework (NPPF)¹ sets out the Government's national policies on different aspects of land use planning in England in relation to flood risk. Planning Practice Guidance (PPG) is also available online².
- 1.4 The PPG sets out the vulnerability to flooding of different land uses. It encourages development to be located in areas of lower flood risk where possible and stresses the importance of preventing increases in flood risk off site to the wider catchment area.
- 1.5 New applications will require a surface water drainage scheme submitted to accompany all planning applications and will be required to demonstrate the use of SuDS within the design and should be in line with the requirements as set out within PPG.
- 1.6 The NPPF states that a site-specific Flood Risk Assessment will be required for proposals:
 - i) that are greater than 1 hectare in area within Flood Zone 1;
 - ii) for all proposals for new development (including minor development and change of use) in Flood Zones 2 and 3;
 - iii) in an area within Flood Zone 1 which has critical drainage problems; and where proposed development or a change of use to a more vulnerable class may be subject to other sources of flooding.

¹ https://www.gov.uk/government/publications/national-planning-policy-framework--2

² https://www.gov.uk/guidance/flood-risk-and-coastal-change



- iv) in an area within Flood Zone 1 identified in a Strategic Flood Risk Assessment as being at increased flood risk in the future.
- v) in an area in Flood Zone 1 that may be subject to other sources of flooding, where its development would introduce a more vulnerable use.
- 1.7 This FRA aims to provide sufficient flood risk information to satisfy the requirements of the NPPF, PPG and regional/local government plans and policies.
- 1.8 This assessment considers the risks of all types of flooding to the site including tidal, fluvial, surface, groundwater, sewer and artificial sources and provides mitigation measures to ensure that the flood risk to the site is minimised and that flood risk off-site is not increased.
- 1.9 This FRA has been based on the following sources of information:
 - NPPF
 - NPPF-PPG
 - Site Layout Plan
 - OS Explorer Series mapping
 - Site Topographical Survey
 - DEFRA Magic mapping
 - Environment Agency mapping
 - Lead Local Flood Authority Guidance
 - Uttlesford Strategic Flood Risk Assessment (May 2016)
 - Site visit undertaken by Cotswold Transport Planning
 - Web Based Soil Mapping
 - British Geological Survey Drift & Geology Maps
 - Anglian Water Sewer Records



2 Existing Site and Hydrology Characteristics

Site Location and Composition

- 2.1 The site is located off Radwinter Road, east of the town of Saffron Walden. The approximate site co-ordinates for the centre of the site are E: 555837; N: 238256, with the nearest post code of CB10 2LB.
- 2.2 The site is located on land classified as Greenfield, with a current arable farmland use, with an approximate area of 18.3 hectares. The site is accessed off Radwinter Road (B1053) which forms part of the site northern boundary.
- 2.3 The site is located east of a residential development off Leverett Way, while agricultural, arable fields surround the southern and eastern areas of the site, bordered by hedgerows.
- 2.4 A minor watercourse flows west through the northern section of the site alongside the existing track present. A small barn is present on the site within the north, located south of the watercourse (see **Appendix A**).
- 2.5 The site location is shown outlined in red in **Figure 2.1**.

Topography

- 2.6 A detailed topographic survey was carried out during March 2021, a copy of which is included within **Appendix A**.
- 2.7 The topographical survey shows ground levels on the site gradually falling to the north west. The highest elevation encountered is 105.17 metres Above Ordnance Datum (mAOD) in the south-eastern corner of the site, and the lowest elevations are around 74.43mAOD in the north-western area of the greenfield element of the site to be built upon, so excluding Radwinter Road.

Ground Conditions

2.8 Geological data held by the British Geological Survey (BGS)³ shows that the bedrock geology underlying the site is Chalk. Superficial deposits of Lowestoft Formation Diamicton are present within the south east of the site (blue area) as shown on Figure 2.2.

³ http://mapapps.bgs.ac.uk/geologyofbritain/home.html

- 2.9 The nearest borehole log is immediately north of the site on the opposite side of the carriageway of Radwinter Road to the site, obtained via online BGS maps. The borehole log reference number is TL53NE9. The log identifies the presence of a shallow depth of sandy clay with underlying chalk.
- 2.10 Soilscapes mapping⁴ indicates the underlying soil as freely draining lime-rich loamy soils.

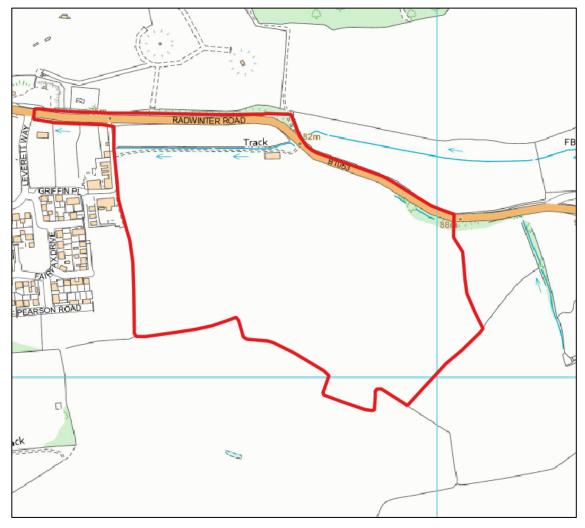


Figure 2.1: Site Location

2.11 Soakaway testing was undertaken during January 2021 by Soils Limited (see Appendix D). A total of two soakaway test pits were established and testing was undertaken in accordance with BRE 365 'Soakaway Design' methodology guidance.

⁴ http://www.landis.org.uk/soilscapes/



- 2.12 The test pits were excavated to depths of 2.000 and 3.400 metres below ground level (mbgl). The borehole logs confirm the soils and geology as depicted by the soils and geology mapping.
- 2.13 Soakaway testing demonstrated low infiltration potential. Groundwater ingress was not encountered, and all sides were stable in both soakaway test pits.
- 2.14 Department for Environment, Food & Rural Affairs (DEFRA) Magic Service Mapping⁵ shows the site is located in a groundwater Source Protection Zone (SPZ). The site is located within the 'Total Catchment' (Zone 3).
- 2.15 These zones show the risk of contamination from any activities that might cause pollution in the area. The closer the activity, the greater the risk. Where infiltration-based SuDS are proposed to manage surface water from a development, then direct discharge into groundwater would not be permissible. Therefore, the elevation of the groundwater table with respect to the base of the soakaway is critical, and there must be an unsaturated zone in the aquifer unit.

⁵ https://magic.defra.gov.uk/MagicMap.aspx



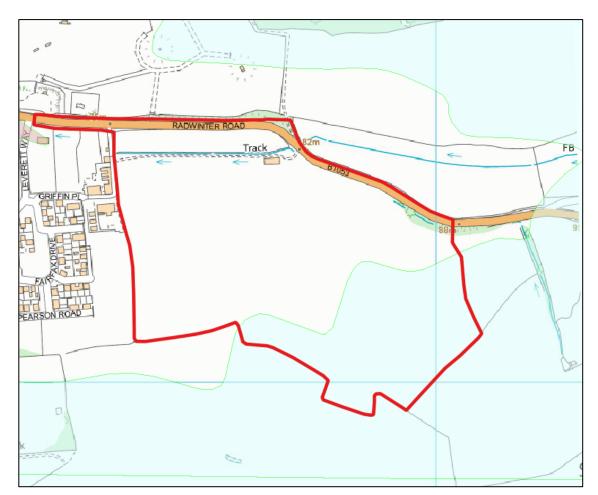


Figure 2.2: Superficial Deposits

Existing Drainage and Hydrology

- 2.16 The closest section of Environment Agency designated Main River (eastern arm of The Slade) is located 567m west of the site. The Slade flows west through Saffron Walden to its confluence with the River Cam approximately 2 miles west of the site at Home Farm.
- 2.17 As mentioned in paragraph 2.4 and shown on **Figure 2.2** above, a minor watercourse flows west through the north of the site. This watercourse issues to the north of Seward's End, circa 743m east of the site and flows west through open farmland before crossing Radwinter Road in culvert and then flowing through the site in open channel. The watercourse then enters an access track culvert before flowing west along the southern side of the carriageway of Radwinter Road as shown on OS mapping to the west of the site.

- 2.18 A further minor watercourse is located 121m to the east of the site, directing flows towards it and then through a narrow area wooded area along the site northern boundary. This watercourse flows into the watercourse crossing the north of the site with the confluence immediately downstream of the Radwinter Road culvert.
- 2.19 Anglian Water asset maps show there is a Foul sewer, 180mm diameter, running east to west along Radwinter Road and then through the northern area of the site, at manhole references 7301, 7302, 6300 and 5300, respectively. Anglian Water sewer records are contained in **Appendix B**.
- 2.20 As the site is classified as Greenfield, it will drain via natural infiltration rates.
- 2.21 The DEFRA Magic Map (England and Wales) shows there are no designated sites (SSSIs) in or close to the site including downstream (from a flood risk and drainage perspective).



3 Proposed Development

Site Proposals

- 3.1 The proposal seeks outline planning permission for the erection of up to 233 residential dwellings including affordable housing, with public open space, landscaping and sustainable drainage system (SuDS) with vehicular access point from Radwinter Road. All matters reserved except for means of access.
- 3.2 A copy of the proposed development drawings is included within **Appendix C**.



4 Development Vulnerability and Flood Zone Classification

National Planning Policy Framework (NPPF)

- 4.1 Local Planning Authorities, (LPA) have a statutory obligation to consult the Environment Agency, (EA) on all applications in flood risk zones. The EA will consider the effects of flood risk in accordance with the NPPF.
- 4.2 NPPF requires that, as part of the planning process:
 - A 'site specific' Flood Risk Assessment will be undertaken for any site that has a flood risk potential.
 - Flood risk potential is minimised by applying a 'sequential approach' to locating 'vulnerable' land uses.
 - Sustainable drainage systems are used for surface water disposal where practical.
 - Flood risk is managed through the use of flood resilient and resistant techniques.
 - Residual risk is identified and safely managed.
- 4.3 Table 1 of NPPF, categorises flood zones into:
 - Zone 1- Low probability (< 1 in 1000 years)
 - Zone 2- Medium probability (1 in 1000 1 in 100 years)
 - Zone 3a- High probability (> 1 in 100 years)
 - Zone 3b- The functional floodplain (>1 in 20 years)
- 4.4 The site is located within Flood Zone 1 as shown on the Environment Agency Flood Map for Planning⁶ and **Figure 5.1**. This is the area shown to be at low risk of river flooding.
- 4.5 The proposed development is considered to be 'more vulnerable' in terms of its land use type flood risk vulnerability as shown in Table 2 of the PPG⁷.
- 4.6 The NPPF sets out a matrix indicating the flood risk vulnerability types of development that are acceptable in different flood zones based upon the Flood Map for Planning as shown in **Table 4.1**.

⁶ https://flood-map-for-planning.service.gov.uk/

⁷ https://www.gov.uk/guidance/flood-risk-and-coastal-change#flood-zone-and-flood-risk-tables



Flood		Flood Risk \	/ulnerability Cla	assification	
Zones	Essential Infrastructure	Highly Vulnerable	More Vulnerable	Less Vulnerable	Water Compatible
Zone 1	✓	\checkmark	\checkmark	✓	✓
Zone 2	√	Exception Test Required	~	~	~
Zone 3a	Exception Test Required	×	Exception Test Required	\checkmark	~
Zone 3b	Exception Test Required	×	×	×	~

Table 4.1: Land Use Vulnerability & Flood Zone Compatibility

Sequential and Exception Test

4.7 The development proposals are classed as 'more vulnerable' within Flood Zone 1 and therefore the Exception Test and Sequential Test are not applicable.



5 Site Specific Flooding

National Planning Policy Framework (NPPF)

- 5.1 In accordance with the National Planning Policy Framework, this Flood Risk Assessment considers all sources of flooding including:
 - Fluvial flooding from rivers and streams;
 - Pluvial flooding overland surface water flow and exceedance;
 - Groundwater flooding from elevated groundwater levels or springs;
 - Flooding from sewers exceedance flows from existing sewer systems; and
 - Artificial sources reservoirs, canals etc.

Historic Flooding

- 5.2 The Strategic Flood Risk Assessment (SFRA) indicates that Saffron Walden has experienced historical flooding, with sources being mainly fluvial and pluvial from The Slade. Bridge Street has been the location of previous flooding incidences as written in the Saffron Walden Reporter⁸.
- 5.3 Saffron Walden has been identified as a Tier 2 area of local flood risk by the Local Lead Flood Authority (Essex County Council), due to the risk presented by surface water flooding⁹.
- 5.4 Historic records of flooding as reported as far back as 1875 for Saffron Walden, with other flood events occurring in 1917, 1960, 2001 and 2014.
- 5.5 Flooding from sewers historically has not presented a high risk, with two properties on the sewer flooding register in Saffron Walden.
- 5.6 The historic flood map available as Open Data from the Environment Agency shows the site is well removed from these historic flood areas.
- 5.7 Consultation undertaken with Essex County Council for flooding information relevant (see Appendix E) identifies there are no records of the site being affected by flooding or a 250m surrounding area.

⁸ Flooding issues in Saffron Walden | Saffron Walden Reporter

⁹ JBA Consulting (uttlesford.gov.uk)



Fluvial Flooding

- 5.8 Flooding from watercourses occurs when flows exceed the capacity of the channel, or where a restrictive structure is encountered, which leads to water overtopping the banks into the floodplain. This process can be exacerbated when debris is mobilised by high flows and accumulates at structures.
- 5.9 The Environment Agency Flood Zones are the current best information on the extent of the extremes of flooding from rivers or the sea that would occur without the presence of flood defences, since these can be breached, overtopped and may not be in existence for the lifetime of a development.
- 5.10 The site is located within Flood Zone 1 as shown on **Figure 5.1**. This is the area shown to be at low risk of river flooding associated with the River Cam and The Slade.
- 5.11 Environment Agency online flood mapping shows that the site does not benefit from flood defences. Although the nearby town of Saffron Walden has historically experienced fluvial flooding, the site is not in a location of historic fluvial flooding, and therefore it is assessed to be at a **low** risk of this flooding source.



Figure 5.1: Flood Map for Planning



Pluvial Flooding

- 5.12 Pluvial flooding can occur during prolonged or intense storm events when the infiltration potential of soils, or the capacity of drainage infrastructure is overwhelmed leading to the accumulation of surface water and the generation of overland flow routes.
- 5.13 Risk of flooding from surface water mapping has been prepared¹⁰, this shows the potential flooding which could occur when rainwater does not drain away through the normal drainage systems or soak into the ground but lies on or flows over the ground instead.
- 5.14 The Surface Water (Pluvial) Flood map provided by the Environment Agency (Figure 5.2) indicates that the site is predominantly at very low risk of pluvial flooding.

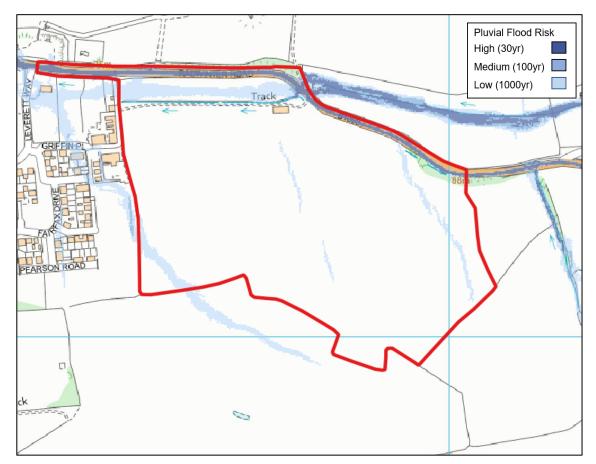


Figure 5.2: Environment Agency Surface Water Flooding Map

5.15 Some areas of potential low risk are shown within the site. Most notably within the north associated with the minor watercourse present.

¹⁰ https://flood-warning-information.service.gov.uk/long-term-flood-risk/map



- 5.16 Overland flow routes (low risk) are present within the south west and east of the site. Shallow depths of flooding (less than 150mm) could occur. To account for this the design of the development at the detailed stage will include for landscaping and road areas to enable the flow paths to remain.
- 5.17 Radwinter Road is identified to be at high risk of pluvial flooding outside the site. Depths of flooding that could potentially be experienced are identified to be circa 300mm. It appears the mapping accounts for the risk of flooding from the minor watercourse culvert crossing surcharging or overtopping onto the carriageway of the road and being directed west and away from the site. The topographical survey displays ground levels to be higher on the site than the adjacent Radwinter Road, which would encourage overland flows on Radwinter Road to flow away from or be contained by the carriageway as opposed to being directed on to the site.
- 5.18 The pluvial maps do not fully represent any underground drainage systems and therefore any flooding entering the site from existing roads is likely to be intercepted by road gullies and discharged into the local drainage network.
- 5.19 Pluvial flood risk for the proposed development is considered to be **low**.
- 5.20 As detailed in Section 7 of this report, the proposed development will not increase surface water flood risk to adjacent land. This is because a surface water drainage strategy has been designed in accordance with Essex County Council guidance and drainage officer liaison.
- 5.21 Whilst it is acknowledged the proposals would result in an increase in runoff generated due to the introduction of impermeable and hardstanding surfaces, the requirement to ensure the rate of runoff discharged from the site is to be restricted to the existing greenfield annual rate. To achieve this onsite storage is proposed within four basins (see **Appendix G**). The strategy will provide an improvement to flood risk by intercepting and controlling runoff from annual to high risk magnitude storm events currently allowed to drain to downstream land at an unrestricted rate.



Groundwater Flooding

- 5.22 Groundwater flooding occurs when the water table rises above ground elevations. It is most likely to happen in low lying areas underlain by permeable geology. This may be regional scale chalk or sandstone aquifers, or localised deposits of sands and gravels underlain by less permeable strata such as that in a river valley.
- 5.23 Mapping available from the Department for Environment, Food & Rural Affairs (DEFRA) Magic Mapping Service¹¹ shows that the site is located in a Principal Bedrock Aquifer, and a Secondary (undifferentiated) Superficial Drift Aquifer.
- 5.24 A Principal Aquifer consists of layers of rock or drift deposits that have high intergranular and/or fracture permeability meaning they usually provide a high level of water storage. They may support water supply and/or river base flow on a strategic scale. In most cases, principal aquifers are aquifers previously designated as major aquifer.
- 5.25 A Secondary Undifferentiated aquifer is assigned in cases where it has not been possible to attribute either category A or B to a rock type. In most cases, this means that the layer in question has previously been designated as both minor and non-aquifer in different locations due to the variable characteristics of the rock type.
- 5.26 The SFRA contains no reference to groundwater flooding at Saffron Walden or close to the area of the proposed development.
- 5.27 Despite the chalk bedrock present in view of the lack of flood history, and the elevation of the site in relation to the wider area, the risk of flooding from groundwater at this stage is considered to be **low**.

Flooding from Sewers

- 5.28 Sewer flooding can occur when the capacity of the infrastructure is exceeded by excessive flows, or as a result of a reduction in capacity due to collapse or blockage, or if the downstream system becomes surcharged. This can lead to the sewers flooding onto the surrounding ground via manholes and gullies, which can generate overland flows.
- 5.29 Anglian Water records indicate there is a 180mm diameter foul water sewer located running east to west, on Radwinter Road and through the north of the proposed site, as shown in sewer records within **Appendix B**.

¹¹ https://magic.defra.gov.uk/MagicMap.aspx



- 5.30 In Saffron Walden, 2 properties on the Anglian Water Sewer Flooding Register are recorded at risk. The SFRA provides no further detail of previous sewer flooding close to the proposed development and as such it can be assumed this source does not contribute a significant risk.
- 5.31 The risk of sewer flooding to the site is therefore considered to be **low.**

Flooding from Artificial Sources

Reservoirs

- 5.32 Flooding can occur from large waterbodies or reservoirs if they are impounded above the surrounding ground levels or are used to retain water in times of flood. Although unlikely, reservoirs and large waterbodies could overtop or breach leading to rapid inundation of the downstream floodplain.
- 5.33 To help identify this risk, reservoir failure flood risk mapping has been prepared¹², this shows the largest area that might be flooded if a reservoir were to fail and release the water it holds. The map displays a worst case scenario and is only intended as a guide.
- 5.34 The EA flood mapping indicates reservoir flooding presents no risk to the site.
- 5.35 The development is considered to be at **negligible** risk of flooding from reservoirs.

¹² https://flood-warning-information.service.gov.uk/long-term-flood-risk/map



6 Flood Mitigation Measures

- 6.1 It is important to demonstrate that future users will not be at risk from flood hazards during the lifetime of the development, as well as ensuring that flood risk is not increased elsewhere.
- 6.2 This assessment has identified that the site is located within Flood Zone 1, which is land assessed as having a less than 1 in 1000 annual probability of fluvial flooding and at low risk. Flood Zone 1 locations are suitable for residential developments as is proposed.

Finished Floor Levels (FFLs)

6.3 It is recommended that FFLs be set a minimum of 150-300mm above the proposed ground levels to provide protection against flooding from surface water runoff.

Ground Levels

- 6.4 Ground levels should be profiled to remove hollows/depressions within the site topography and the area of potential risk of pluvial flooding.
- 6.5 Ground levels should be finished so that existing overland flow routes are preserved, and overland runoff is encouraged to flow away from the proposed new buildings and be directed to the nearest on site drainage system runoff collection point.

Access and Egress

- 6.6 Safe pedestrian access/egress is available onto Radwinter Road in order to access the wider road/street network to the north of the site. This is due to the Flood Zone 1 designation of the site and surrounding adjacent land.
- 6.7 It is acknowledged that pluvial flooding could pose a risk, however, the depths that could be encountered during a high risk event are shallow, with a maximum potential depth of 300mm and could be waded through if required.

Groundwater

6.8 The potential for shallow groundwater should also be considered during the construction phase of the development, particularly during the excavations. It is recommended that groundwater levels are monitored during the construction phase, and where groundwater is encountered appropriate dewatering should be employed.



Drainage

6.9 To mitigate the proposed developments impact on the current runoff regime through the increased rate of runoff that would result due to the impermeable areas to be introduced; it is proposed to incorporate surface water attenuation and storage as part of the development proposals as discussed in paragraphs 5.20-5.21. The proposed drainage strategy is further detailed in Section 7.

Consents

6.10 It is recognised that as a new access crossing is proposed, a Land Drainage Consent from the Lead Local Flood Authority is likely to be required through the terms of the Land Drainage Act, 1991 (Section 23) for works affecting the flow of 'ordinary watercourses'. This is an approval process that is separate to obtaining planning approval.



7 Proposed Drainage Strategy

- 7.1 Consideration of flood issues is not confined to the floodplain. This is recognised in the NPPF and associated guidance. The alteration of natural surface water flow patterns through developments can lead to problems elsewhere in a catchment, particularly flooding downstream; and replacing permeable vegetated areas with low permeability roofs, roads and other paved areas will increase the speed, volume and peak flow of surface water runoff.
- 7.2 A surface water management strategy for the development is proposed to manage and reduce the flood risk posed by surface water runoff from the site. The surface water drainage arrangements for any development site should be such that the volume and peak flow rates of surface water leaving a developed site are no greater than the rates prior to the proposed development unless specific off-site arrangements are made and result in the same net effect.
- 7.3 An assessment of the surface water runoff rates was undertaken to determine the surface water options and attenuation requirements for the site and is discussed below.

Surface Water Management

- 7.4 Sustainable drainage system measures (SuDS) should be used to control the surface water runoff from the proposed development site, thereby managing the flood risk to the site and surrounding area from surface water runoff. These measures will also improve the quality of water discharged from the site.
- 7.5 The SuDS hierarchy demands that surface water runoff should be disposed of as high up the following list as practically possible:
 - Into the ground (infiltration) and re-use, or then;
 - To a surface water body, or then;
 - To a surface water sewer, highway drain or another drainage system, or then;
 - To a combined sewer.
- 7.6 The underlying bedrock geology of the site is Chalk. Whilst Chalk is considered to be permeable in nature, infiltration testing conducted on the site confirmed the use of soakaway drainage is not a viable solution for surface water disposal (see Appendix D).



7.7 It is therefore proposed to discharge flows of generated surface water runoff into the minor watercourse flowing west, located within the north of the site.

Greenfield Runoff and Required Storage Volumes

7.8 Greenfield rates calculated from MicroDrainage Source Control (see outputs included within **Appendix F**) for the proposed developable area (6.52ha) are as follows:

Return Period (Yrs)	Runoff Rate (I/s)
1	20.8
QBAR	23.9
30	57.5
100	85.1

Table 7.1: Greenfield Runoff Rates

7.9 It is recognised Essex County Council as the LLFA for the area require flow restriction to the 1 in 1 year greenfield rate.

Proposed Drainage

- 7.10 The introduction of hardstanding associated with the proposed development will introduce a developable area totalling 6.52ha, which will increase the amount of runoff generated and could increase flood risk elsewhere unless managed in accordance with Essex County Council guidance.
- 7.11 Based on the proposed restriction to the 1 in 1 year runoff rate, an attenuation volume of approximately 2700m³ is required, calculated on the assumption that 65% of the developable area would become impermeable surfacing with positive drainage. This figure accounts for an assumed 55% impermeable area with 10% to account for future urban creep.
- 7.12 The primary attenuation and sustainable drainage (SuDs) features proposed comprise of four basins attenuated via final controls and throttle pipes, with a maximum water level of 1.2m. A Hydro-brake control chamber is also proposed to restrict flows out of attenuation basin 4 to 20.8l/s. There are also three SuDS corridors proposed, which will include for swales, two of which, will follow the line of the existing oil pipelines present crossing the site.
- 7.13 To demonstrate that the necessary storage volumes can be accommodated on the site an illustrative drainage layout has been prepared and has been included as Appendix
 G. Supporting drainage calculations are included in Appendix F. Details of the proposed



drainage approach and storage requirements are also summarised within **Appendix H** and the completed technical appendix proforma required to support the planning application.

7.14 The final layout and design of the surface water drainage network will be determined at the detailed design stage as the development masterplan evolves.

Exceedance Events

- 7.15 The detention basins will be designed with a capacity up to a 1 in 100-year (plus 40% climate change) event, with a +300mm freeboard allowance, based on the 28.8l/s restricted discharge rate. This provides a betterment (reduction) in runoff when compared to existing undeveloped conditions, where runoff is uncontrolled across all return periods.
- 7.16 A storm event in excess of this design standard would be extreme and would cause the detention basin to overtop (with no sudden deluge) and would then shed overland following the topography of the site, as per existing conditions.
- 7.17 Finished floor levels of new dwellings will be set above external levels, which will mitigate the residual risk of overtopping.

Water Quality

7.18 It is acknowledged that SuDS can be incorporated into the stormwater strategy to provide water quality measures. It is intended that surface water will be drained via a traditional gravity system and directed to SuDS features. The concept is for surface water to navigate through two or more SuDS features to provide water quality treatment and attenuate.

Foul Water Management

7.19 Foul water from the development shall be collected through a traditional gravity drainage system and directed to a connection with the 180mm diameter foul sewer on Radwinter Road, as confirmed by Anglian Water.

Maintenance Regime

7.20 Maintenance of SuDS features are essential to ensure that the surface water drainage system operates effectively and that flooding of the site and surrounding areas is prevented.



- 7.21 The responsibility of maintaining the private surface water and foul water drainage components would lie with the landowner of the site, who may delegate responsibility to an appointed external private management company.
- 7.22 For all drainage aspects a full maintenance regime should be carried out (see Table 7.2) to ensure that drainage systems remain operational in accordance with manufacturer's guidelines and drainage features maintenance requirements as set out in the SuDS Manual (C753).

Drainage Component	Required Action	Typical Frequency
	Stabilise adjacent areas	As required
Dinowork	Remove weeds	As required
Pipework, manholes,	Clear any poor performing structures.	As required
flow control chambers,	Inspect all structures for poor operation	Three monthly, 48 hours after large storms in first six months
catch pits and silt traps	Monitor inspection chambers. Inspect silt accumulation rates and determine silt clearance frequencies	Annually
	Inspect and identify any areas that are not operating correctly. If required, take remedial action	Monthly for 3 months, then annually.
	Remove debris from the catchment surface (where it may cause risks to performance)	Monthly
Attenuation Tank	Inspect inlets, outlets, banksides, structures, Repair/rehabilitate inlets, outlet, overflows and vents	As Required
	Inspect/check all inlets, outlets, vents and overflows to ensure that they are in good condition and operating as designed.	Annually
	Survey inside of tank for sediment build-up and remove if necessary	Every 5 years or as required.

Table 7.2: Initial Operation and Maintenance Plan



8 Summary and Conclusion

- 8.1 Cotswold Transport Planning were appointed by Rosconn Strategic Land to produce a Flood Risk Assessment (FRA) for an outline residential proposal of up to 233 dwellings on Land South of Radwinter Road (East of Griffin Place), Saffron Walden.
- 8.2 This assessment has considered the risks of all types of flooding to the site including tidal, fluvial, surface, groundwater, sewer and artificial sources and provides mitigation measures to ensure that the flood risk to the site is minimised and that flood risk off-site is not increased.
- 8.3 The proposed development is classified as 'more vulnerable' and is located within a site identified to be within Flood Zone 1 and therefore does not require application of the Sequential or Exception Tests.
- 8.4 The site is considered to be at low risk of flooding from fluvial, pluvial, groundwater and sewer sources.
- 8.5 The site is considered to be at negligible risk of flooding from artificial sources.
- 8.6 Safe pedestrian access and egress is available onto Radwinter Road in order to access the wider road/street network to the north of the site and land outside the floodplain.
- 8.7 Surface water runoff generated by the proposal will be stored on site using attenuation basins and SuDS corridors, before discharging into the existing watercourse via a Hydrobrake control chamber to the west of the site. This formalised approach to controlling runoff will assist in reducing downstream flood risk.
- 8.8 Foul drainage is proposed to connect into the existing public foul sewer on Radwinter Road, confirmed by Anglian Water.
- 8.9 In compliance with the requirements of the National Planning Policy Framework, and subject to the mitigation measures proposed, the development could proceed without being subject to significant flood risk.

Appendix A

Topographical Survey

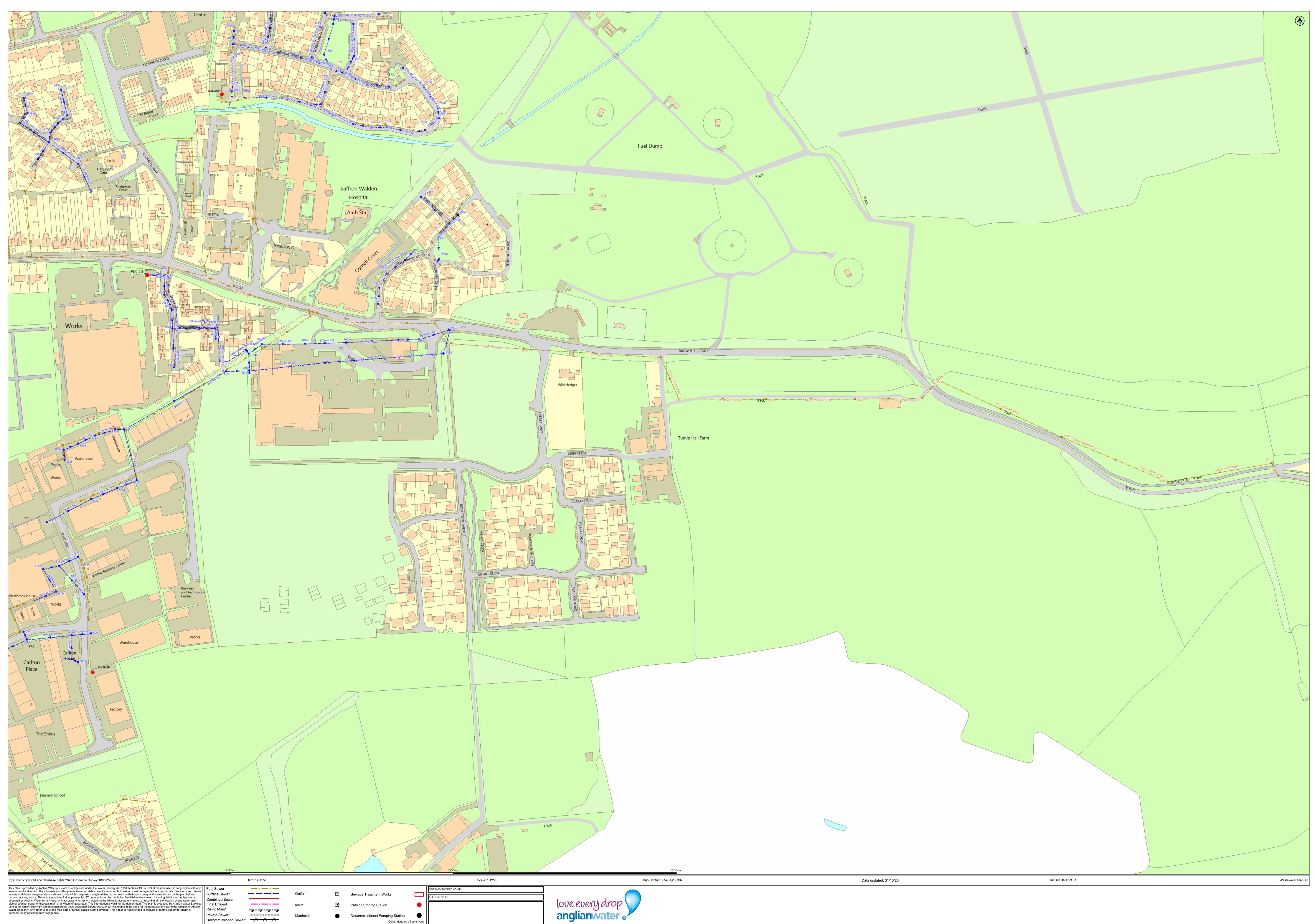


+	SurveyKey:B0BollardBBBelisha BeaconBTBT CoverCBTelephone Control BoxCHCoal HoleCOUnidentified CoverConcConcreteEPElectricity PoleFHFire HydrantFTFace Profile TargetFWFoul Water Drain CoverGUDrainage Gully CoverGVGas CoverICInspection Chamber CoverLBLetter BoxLPLamp PostMCMetal Drainage ChannelMHManhole Cover (round)MPMarker PostRwpRain Water Drain CoverTCBTelephone Call BoxTLTraffic LightTPTelegraph PoleTVCable TV CoverWMWater Meter Cover
	STN M57.08Survey Control StationIP 154.87Trial PitImage: BH 154.87BoreholeWL 154.87 21/01/10Water Level (with date measured)+ 154.87 (with date measured)+ 154.87 (mith date measured)- 154.87 (mith date measured)
	Linetypes Fenceline Fenceline Electricity Transmission Line Hedge Rock Face Embankment Slope Contour Lines Gas Pipeline Water Pipeline
	Building Internals – Specific Codes Ceil 154.87 + 154.87 Structural Ceiling Level F-Ce + 154.87 + 154.87 Floor Level Usb + 154.87 + 154.87 Underside of Beam / Openings Level Some of these symbols may not appear on this drawing
	(c) The Intellectual Copyright of the data in this drawing belongs to Beacon Land Surveys Limited 2021
	Beacon an Surveys The Lodge Greenhough Road Lichfield Staffs. WS13 7AU Tel : 01543 417399 Mob: 07764 585084 email :-
	Project: Land off Radwinter Road Drawing: Land ES€€ăil & Level Survey
Notes :— Survey is tied to Ordnance Survey grid and level by GPS Smartnet L Contours are shown at 0.5m intervals and highlighted at 2m interva	Scales: 1:1000 Drawn/Sheet Size: mjs/A1 Date: Drawing No:

20-103-2

Appendix B

Anglian Water Sewer Records



0200	556052	238263	F	90.28	87.89	2.39
0401 0402	555022 555088	238473 238455	F F	67.26 67.93	65.4 65.959	1.86 1.971
0403	555090	238449	F	69.21	66.1	3.11
0404 0405	555039 555097	238415 238453	F F	72.58 67.93	69.32 66.99	3.26 0.94
0500	555027	238559	F	-	-	-
0501 0502	555007 555031	238525 238546	F F	-	-	-
0600 0601	555086 555065	238690 238696	F	-	-	-
0601	555018	238696	F	-	-	-
0603 0700	555031 555001	238613 238714	F F	-	-	-
0700	555001	238714	F	-	-	-
0702 0703	555005 555006	238756 238765	F F	-	-	-
0703 0704	555093	238705	F	-	-	-
0705 0706	555068 555045	238743 238748	F F	-	-	-
1200	556176	238270	F	92.77	90.861	1.909
1201 1400	556169 555130	238284 238442	F F	93 69.47	89.361 66.804	3.639 2.666
1401	555169	238479	F	-	-	-
1402 1403	555177 555167	238496 238442	F F	-	-	-
1500	555194	238508	F	-	-	-
1600 1601	555104 555102	238689 238684	F F	-	-	-
1602	555175	238664	F	-	-	-
1603 1604	555155 555142	238663 238666	F F	-	-	-
1700	555108	238787	F	-	-	-
1701 1702	555125 555165	238787 238785	F F	-	-	-
1703	555177	238785	F	-	-	-
1704 1705	555195 555186	238714 238708	F F	-	-	-
1706	555153	238708	F	-	-	-
1707 1708	555133 555120	238721 238727	F	-	-	-
1709	555111	238710	F	-	-	-
2400 2401	555248 555229	238418 238441	F	71.2 69.99	68.563 67.82	2.637 2.17
2401 2402	555229 555268	238441 238497	F	- -	-	-
2500 2501	555223 555227	238518 238532	F	-	-	-
2501 2502	555227	238532 238556	F	-	-	-
2503	555230	238572	F	-	-	-
2504 2505	555253 555260	238563 238575	F F	-	-	-
2506	555235	238507	F	-	-	-
2507 2600	555253 555238	238507 238659	F F	-	-	-
2601	555221	238656	F	-	-	-
2602 3400	555206 555330	238657 238412	F F	- 71.86	- 69.5	- 2.36
3401	555305	238496	F	-	-	-
4400 5300	555483 555503	238403 238356	F F	75.2 77.15	72.413 73.038	2.787 4.112
6300	555601	238356	F	78.16	73.705	4.455
7002 7101	554764 554753	238095 238121	F F	78.07 78.3	74.79 75.29	3.28 3.01
7102	554768	238126	F	79.6	78.17	1.43
7300 7301	555794 555776	238377 238357	F F	82.14 81.75	78.944	3.196 4.706
7302	555701	238356	F	79.82	75.372	4.448
7502 7503	554788 554777	238515 238515	F	63.24 63.25	60.83 60.96	2.41 2.29
7504	554774	238550	F	-	61.14	-
7505 7506	554770 554752	238589 238519	F F	-	61.43	-
7507	554752	238533	F	-	-	-
7603	554781	238604	F	-	61.55	-
7604 7605	554782 554797	238619 238640	F F	-	61.64 61.81	-
7606	554762	238665	F	-	63.65	-
7607 7608	554770 554766	238676 238691	F F	-	64.02 65.23	-
7703	554755	238780	F	72.66	70.68	1.98
7704 7801	554758 554781	238753 237853	F F	70.55 77.48	68.76 75.97	1.79 1.51
7802	554776	237857	F	77.24	75.75	1.49
7803 7804	554798 554773	237864 237860	F F	79.32 76.72	77.94 75.42	1.38 1.3
7810	554760	237859	F	-	-	0.92
7811 8101	554752 554841	237850 238108	F F	- 83.99	- 82.28	1.045 1.71
8102	554839	238156	F	82.48	79.98	2.5
8103 8201	554833 554862	238175 238255	F F	81.31 76.6	80.21 74.12	1.1 2.48
8202	554832	238242	F	77.21	74.65	2.56
8203 8204	554894 554815	238270 238290	F F	76.17 74.49	73.51 72.84	2.66 1.65
8205	554807	238287	F	74.59	72.98	1.61
8301 8302	554883 554853	238321 238318	F F	73.61 73.84	71.61 72.11	2 1.73
8303	554812	238304	F	74.28	72.74	1.54
8304 8501	554869 554879	238325 238516	F F	73.59 64.93	71.84 61.22	1.75 3.71
8600	554829	238617	F	-	62.07	-
8601 8602	554849 554868	238630 238635	F F	-	62.22 62.32	-
8603	554800	238658	F	-	-	-
8604 8605	554821 554818	238672 238637	F F	-	62.8 -	-
8701	554838	238772	F	-	-	-
8702 8802	554813 554868	238700 237891	F F	- 84.3	64.85 83.09	- 1.21
8803	554854	237883	F	83.22	82.24	0.98
8901 9300	554880 555934	237907 238313	F F	85.89 85.5	84.63 83.49	1.26 2.01
9301	554947	238358	F	73.16	70.78	2.38
9302 9303	554996 554939	238389 238394	F F	72.83	70 -	2.83 -
9401	554973	238494	F	66.36	61.59	4.77
9402 9403	554978 554927	238491 238478	F F	66.43 -	-	-
9404	554929	238472	F	-	-	-
9405 9406	554964 554938	238434 238434	F F	-	-	-
9407	554984	238434	F	-	-	-
9408 9409	554936 554930	238460 238498	F F	-	-	-
9500	554931	238504	F	-	-	-
9501 9502	554959 554959	238578 238565	F F	-	-	-
9503	554971	238506	F	-	-	-
9504 9600	554978 554990	238526 238690	F F	-	-	-
9601	554999	238689	F	-	-	-
9602 9603	554926 554957	238648 238649	F F	-	-	-
9604	554958	238619	F	-	-	-
9901 0351	554909 555021	237904 238388	F S	88.01 73.371	86.75 71.371	1.26 2
0352	555021	238388 238385	S	73.371	71.379	1.992
0451	555084	238418	S	74.121	70.276	3.845
0452 0453	555035 555021	238418 238407	S S	72.371 73.09	71.096 71.39	1.275 1.7
0454	555018	238411	S	-	-	-
0650	555090 555064	238686 238693	S S	-	-	-
	555016	238695	S	-	-	-
0651 0652		238695	S	-	-	-
0651 0652 0653	555002 555004	238769	S	_	-	-
0651 0652 0653 0750 0751	555004 555003	238769 238754	S	-	-	-
0651 0652 0653 0750	555004	238769		-	-	

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	0756	555040	238751	S -		-	-								
						-	-								
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	1452	555189	238422	S 72.											
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Manhole Reference	Easting	Northing	Liquid Type	Cover Level	Invert Level	Depth to Invert	Manhole Reference	Easting	Northing	Liquid Type	Cover Level	Invert Level	Depth to Invert
													Ref: 459393 - 1

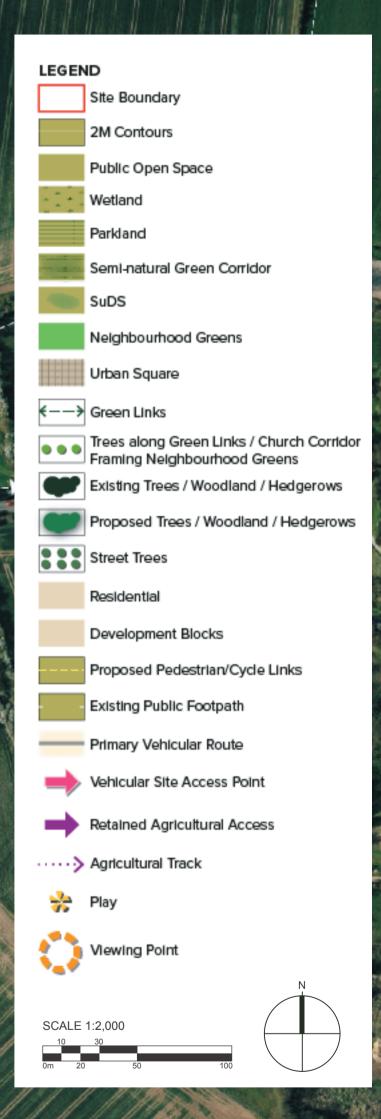
Our Ref: 459393 - 1

Appendix C

Proposed Development Plans







M	Rev
DE_436-005	Drg No
Rosconn Ltd	Client
Saffron Walden	Project
Illustrative Masterplan	Title
1:2,000@A2	Scale

Appendix D

Soakaway Testing Results

Soakaway Calculations

Soakaway Test No.	INF 01
Contract:	Saffron Waldon
Contract No.	18948

Trial Pit Log (include details of groundwater):
See trial Pit record

Depth of Pit	2.00 m
Width of Pit	0.60 m
Length of Pit	2.50 m
Depth of Pit Soaked	0.80 m
ap50	3.98 m2
Vp75-25	0.6 m3
t75-25	0.0 min
water used	1.2000 m3
f	#DIV/0! m/sec.

Field Data

Depth to	Elapsed	Head of	Head of		T75	Τ2	25	
Water	Time	Water	Water					
(m)	(min)	(% of Ho)	(m)	100 🛑			_	
1.00	0	100	1		•			
1.00	1.0	100	1.00					
1.00	2.0	100	1.00	90 +				
1.00	3.0	100	1.00					
1.00	4.0	100	1.00					
1.00	5.0	100	1.00	80 +				
1.00	10.0	100	1.00					
1.03	28.0	97	0.97	. U				
1.03	118.0	97	0.97	70 +				
1.03	154.0	97	0.97					
1.03	177.0	97	0.97					
				60 +				
				<u> </u>				
				Head (% of Ho)				
				• 50 +				
				0				
				ead				
				 .				
				40				
				30 -				
				. 30 -				
				. 6				
				20 +				
				10 +				
75	0.000	75		0 +				
25	0.000	25		0.0	50.0	100.0	150.0	200.0
75-25	0.000	Derived from	Best Fit		Elap	osed Tir	ne (min)	
comment				-				
Extrapolat	ed past 12	0mins						
		oad, Tadworth		Te	elephone:	01737 81	4 221	
urrey, KT2		,			01737 81			

Soakaway Calculations

Soakaway Test No.	Groundwater Pit
Contract:	Saffron Waldon
Contract No.	18948

Field Test

Trial Pit Lo	g (include details of groundwater):
See trial Pit re	ecord

Depth of Pit	3.40 m
Width of Pit	0.60 m
Length of Pit	2.60 m
Depth of Pit Soaked	0.80 m
ap50	4.12 m2
Vp75-25	0.624 m3
t75-25	0.0 min
water used	1.2480 m3
f	#DIV/0! m/sec.

Field Data

Depth to	Elapsed	Head of	Head of	_	T75	T2	25	
Water	Time	Water	Water	-				
(m)	(min)	(% of Ho)	(m)	100				
2.20	0	100	1.2					
2.20	1.0	100	1.20		L			
2.30	2.0	92	1.10	90 +				
2.30	3.0	92	1.10	_				
2.30	4.0	92	1.10	_			ľ	
2.30	5.0	92	1.10	80 +				
2.30	8.0	92	1.10	-				
2.31	13.0	91	1.09	- Ĭ				
2.33	55.0	89	1.07	70 +				
2.33	90.0	89	1.07	_				
2.34	145.0	88	1.06	-				
2.4	175.0	83	1.00	60 +				
				<u>ି</u> ବି				
				Head (% of Ho) + 050 + 00				
				- <u>≈</u> 50 +				
				- 0				
				ea.				
				- エ _{40 +}				
				-				
				-				
				- 30 -				
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				<u>-</u> 9				
				- 20 +				
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				- 10 +				
				-				
				-				
75	0.000	75		- 0 -				
25	0.000	25		0.0	50.0	100.0	150.0	200.0
75-25		Derived from	Bost Fit	- 0.0				200.0
10-20	0.000	Derived HUIII	Destrit	-	Elä	apsed Tii	ne (min)	
Comment	ts							
	ed past 12	Omins						
-/// upolai	ou puot 12							
		oad, Tadworth		Te	elephone:	01737 81	4 221	
urrey, KT2		ouu, iuumoitii			acsimile:	01737 81		

SO		Ne Tel:	Sc wton House, Cro 01737 814221 E	o ils Limi ss Road, mail: adm	Tadwort	h KT20 5S slimited.co	SR .uk	Tri	al Pit Log	Trial Pit No. Groundwa er Sheet 1 of 1
	Name: Saf	fron Wald	on		Proiec	t No.: 18	948	Method:		Hole Type
Locatior		fron Wald						Plant:	5 Ton Swingshovel	TP
								Support:	T	Scale 1:25
Client:	C/O		Tranport and Pla	nning		Iri	al Pit Leng		Trial Pit Width: 0.60m	Logged By
Dates:		18/01		Level:			Co-oro	ds:		KC
Water Strike	Sam Depth	ples & In S	Situ Testing Results	Depth (m)	Level (mAOD)	Legend			Stratum Description	
500	Deptil	Type	Results	()	(11/ (02)		Brown sli	ghtly sandy SI	LT with frequent rootlets. (Top	soil)
	0.25 0.50	D		0.20			medium. lithologie Firm brov	Gravel is subro s. (Head) wn slightly sand	y slightly gravelly CLAY. Sand bunded to round, medium of v dy gravelly CLAY. Sand is fine led of flint. (Head)	arious - - - - -
	1.00	D								
	1.50	D								
	2.00	D		2.20			Dense C	HALK with fine	to coarse, sub-angular to sub	-rounded
	3.00	D					GRAVEL	of flint.		- - - - - - - - - - - - - - - - - - -
				3.40					End of Pit at 3.400m	
										- - - - - - - - - - - - - - - - - - -
Groundwa	Remarks: ater not encc ater Remark:		l sides stable.							Sample Type D: Disturbed B: Bulk J: Jar W: Water

6	Sile				ils Limit					.			Trial Pit N	
		D	l Te	Newton House, Cro el: 01737 814221 E	ss Road, mail: adm	Tadwortl iin@soils	h KT20 slimited) 5SR 1.co.uk		Iri	al Pit Lo	bg	INF0 ² Sheet 1 o	
Projec	ct Name:	Saffr	on Wa	ldon		Projec	t No.:	18948		lethod:	E Tono Swing	abayal	Hole Typ TP	
Locati	ion:	Saffr	on Wa	ldon						lant: upport:	5 Tone Swing	snovei	Scale	
Client	:	c/o C	otswo	ld Tranport and Pla	nning			Trial Pit Len	igth:	2.50m	Trial Pit Width:	0.60m	1:25	<u></u>
Dates	:		18/0	01/2021	Level:			Co-c	ords:		•		Logged E JO	зу
/ater trike				n Situ Testing	Depth		Legen	d		:	Stratum Descriptio	'n		
Water Strike saped					4	Level (mAOD)		d Brown s Firm bro medium lithologi	slight own n. Gra ies. (own	tly sandy Sll slightly andy avel is subre (Head) slightly sand se, subround	Stratum Descriptio	otlets. (Topso	ine to	
														- 5
	al Remarks Iwater not e		ntered.	All sides stable.		1	1						Sample Type D: Disturbed	
Groups	lwater Rem	Jarko:											B: Bulk J: Jar W: Water	
Sibund		iai NS.												

Appendix E

Essex County Council Flooding Information

Essex County Council **Environment and Planning** Flood and Water Management Team E3 County Hall Chelmsford CM1 1QH



Ben Fleming

Date: 30/04/2021

Dear Mr Fleming,

Basic information request for data held by LLFA - Land south of Radwinter Road Saffron Walden CB10 2LB

Thank you for contacting us for information held on the above site. I have checked our records for reported surface water flooding in the area you have provided on your plans.

The majority of the site in question is shown to be at a very low risk of surface water flooding with small areas of low risk around the ordinary watercourse within you site, according to the gov.uk 'flood risk from Surface Water' map. Further information can be found on the Gov.uk website: <u>https://flood-warning-information.service.gov.uk/long-term-flood-risk/map.</u>



Figure 1: Flood risk from surface water - Land south of Radwinter Road Saffron Walden CB10 2LB

Surface Water Management Plans

The Surface Water Management Plan (SWMP) produces more detailed modelling and identifies Critical Drainage Area's (CDA); highlighting areas most at risk. Essex County Council has not yet completed a SWMP including your site.

Watercourses and rivers

Analysis has been completed using all of our data sets to a distance of 250m from the aforementioned site and within the site boundaries itself, as detailed in Figure 2 below.



Figure 2: Site plan including 250m 'buffer zone'



(c) Copyright.

The search has confirmed that there are two ordinary watercourses within your site as shown in figure 2 with the green line. It is situated along the northern boundary of your site and runs west to east. For any information on main rivers you should contact the environment agency on the email below: <u>enquiries@environment-agency.gov.uk</u>

It should be noted that smaller watercourses are not always mapped, therefore site investigation should be carried out to verify information supplied.

If proposed works entail temporary or permanent alterations to a watercourse, consent will be required. Essex County Council does offer a pre-application advice facility whereby one of our engineers will review your proposed works and offer engineering advice should it be required. Further information can be found on our website using the following link:

http://flood.essex.gov.uk/change-a-watercourse/apply-for-a-watercourse-consent/

Flood risk assets

Our database has confirmed that there are no flood assets within your site and the 250m buffer zone. As with smaller watercourses, not all flood risk assets will be mapped so further investigation is advised.

Flood Incidents and Investigations

Our database has confirmed that there are no records of any flood incidents within your site and the 250m buffer zone.

In respect of Sustainable Drainage, we have not received any sustainable drainage consultations within your site or the 250m buffer zone. For further drainage and discharge information, please visit <u>https://flood.essex.gov.uk/new-development-advice/apply-for-suds-advice/</u>.

- We have no records of any historic flooding in this area.
- For information regarding sewers and groundwater, please contact the Environment Agency.

I would note however that we only have a limited number of records as we have only been a Lead Local Flood Authority since 2010. Whilst we are working to build a comprehensive database of flood incidents, unlike main rivers we have no formal system of monitoring water levels and being aware when flooding occurs. We rely on reports from residents and in particular district councils to report flood incidents to us. As such all we can provide is an indication of the flood history that we have available to us, if we have no recorded incidents then it does not necessarily mean that flooding has never occurred there, merely that it has not been reported to us.

I hope that the above assists you with your enquiry.

Yours sincerely,

Amanda Rossell Essex County Council Flood and Water Management Team

Please reply to:	Flood & Water Management Team
Email:	floods@essex.gov.uk
Internet:	www.essex.gov.uk/flooding

Appendix F

Drainage Calculations

Cotswold Transport Planning		Page 1
CTP House, Knapp Road		
Cheltenham		
Gloucestershire, GL50 3QQ		Micro
Date 19/06/2021 13:10	Designed by NicolaTiley	
File 20-1142_QBAR AND ATTEN.SRCX	Checked by	Drainage
Innovyze	Source Control 2020.1	
Return Period (years) Area (ha) 6	100 SAAR (mm) 600 Urban 0.000 .520 Soil 0.450 Region Number Region 5	
	Results 1/s	
	QBAR Rural 23.9	
	QBAR Urban 23.9	
	Q100 years 85.1	
	Q1 year 20.8 Q30 years 57.5 Q100 years 85.1	

Cotswold Transport Planning					
CTP House, Knapp Road	CTP-20-1142 Saffron Walden	Page 1			
Cheltenham	Attenuation requirements				
Gloucestershire, GL50 3QQ	Up to 1 in 100 Year + 40% CC	— Micro			
Date 19/06/2021 13:14	Designed by NT	Drainage			
File 20-1142_QBAR AND ATTEN.SRCX	Checked by KT	Diamaye			
Innovyze	Source Control 2020.1				

Summary of Results for 100 year Return Period (+40%)

Storm Event			Max Level (m)	Max Depth (m)	Max Control (l/s)	Max Volume (m³)	Status
15	min	Summer	78.430	0.430	20.8	1103.5	ОК
30	min	Summer	78.547	0.547	20.8	1420.9	0 K
60	min	Summer	78.658	0.658	20.8	1729.2	0 K
120	min	Summer	78.757	0.757	20.8	2009.8	Flood Risk
180	min	Summer	78.805	0.805	20.8	2147.4	Flood Risk
240	min	Summer	78.832	0.832	20.8	2224.8	Flood Risk
360	min	Summer	78.857	0.857	20.8	2297.8	Flood Risk
480	min	Summer	78.866	0.866	20.8	2325.2	Flood Risk
600	min	Summer	78.866	0.866	20.8	2324.4	Flood Risk
720	min	Summer	78.859	0.859	20.8	2306.1	Flood Risk
960	min	Summer	78.837	0.837	20.8	2239.8	Flood Risk
1440	min	Summer	78.790	0.790	20.8	2105.2	Flood Risk
2160	min	Summer	78.727	0.727	20.8	1923.5	Flood Risk
2880	min	Summer	78.664	0.664	20.8	1746.5	0 K
4320	min	Summer	78.547	0.547	20.8	1420.9	O K
5760	min	Summer	78.447	0.447	20.8	1149.3	O K
7200	min	Summer	78.361	0.361	20.8	918.3	0 K
8640	min	Summer	78.288	0.288	20.8	726.8	0 K
10080	min	Summer	78.230	0.230	20.8	576.3	0 K
15	min	Winter	78.481	0.481	20.8	1239.5	0 K
30	min	Winter	78.611	0.611	20.8	1597.2	O K
60	min	Winter	78.735	0.735	20.8	1946.1	Flood Risk
120	min	Winter	78.846	0.846	20.8	2266.9	Flood Risk
180	min	Winter	78.901	0.901	20.8	2427.8	Flood Risk
240	min	Winter	78.933	0.933	20.8	2521.4	Flood Risk

	Stor		Rain		Discharge	
	Even	C	(mm/hr)	Volume (m³)	Volume (m ³)	(mins)
				()	(111)	
15	min	Summer	142.716	0.0	1132.8	30
30	min	Summer	92.222	0.0	1464.3	45
60	min	Summer	56.713	0.0	1801.4	74
120	min	Summer	33.722	0.0	2141.8	132
180	min	Summer	24.576	0.0	2341.8	192
240	min	Summer	19.534	0.0	2482.4	250
360	min	Summer	14.061	0.0	2680.5	368
480	min	Summer	11.142	0.0	2832.0	486
600	min	Summer	9.297	0.0	2953.6	604
720	min	Summer	8.015	0.0	3055.9	722
960	min	Summer	6.338	0.0	3164.9	922
1440	min	Summer	4.546	0.0	3118.1	1146
2160	min	Summer	3.257	0.0	3726.2	1540
2880	min	Summer	2.568	0.0	3916.6	1944
4320	min	Summer	1.836	0.0	4200.1	2724
5760	min	Summer	1.445	0.0	4409.1	3464
7200	min	Summer	1.200	0.0	4576.1	4184
8640	min	Summer	1.031	0.0	4717.3	4856
10080	min	Summer	0.906	0.0	4837.6	5552
15	min	Winter	142.716	0.0	1268.8	30
30	min	Winter	92.222	0.0	1616.7	44
60	min	Winter	56.713	0.0	2017.9	74
120	min	Winter	33.722	0.0	2399.9	130
180	min	Winter	24.576	0.0	2623.2	188
240	min	Winter	19.534	0.0	2780.0	246

Cotswold Transport Planning					
CTP House, Knapp Road	CTP-20-1142 Saffron Walden				
Cheltenham	Attenuation requirements				
Gloucestershire, GL50 3QQ	Up to 1 in 100 Year + 40% CC	Micro			
Date 19/06/2021 13:14	Designed by NT	Drainage			
File 20-1142_QBAR AND ATTEN.SRCX	Checked by KT	Diamage			
Innovyze	Source Control 2020.1				

Summary of Results for 100 year Return Period (+40%)

Storm Event		Max Level (m)	Max Depth (m)	Max Control (l/s)	Max Volume (m³)	Status	
360	min	Winter	78.965	0.965	20.8	2616.6	Flood Risk
480	min	Winter	78.979	0.979	20.8	2660.5	Flood Risk
600	min	Winter	78.983	0.983	20.8	2671.9	Flood Risk
720	min	Winter	78.980	0.980	20.8	2663.4	Flood Risk
960	min	Winter	78.963	0.963	20.8	2611.0	Flood Risk
1440	min	Winter	78.906	0.906	20.8	2443.6	Flood Risk
2160	min	Winter	78.830	0.830	20.8	2219.0	Flood Risk
2880	min	Winter	78.751	0.751	20.8	1992.0	Flood Risk
4320	min	Winter	78.577	0.577	20.8	1504.3	ОК
5760	min	Winter	78.425	0.425	20.8	1089.5	ОК
7200	min	Winter	78.299	0.299	20.8	757.1	ОК
8640	min	Winter	78.204	0.204	20.7	511.7	O K
10080	min	Winter	78.139	0.139	20.2	346.5	0 K

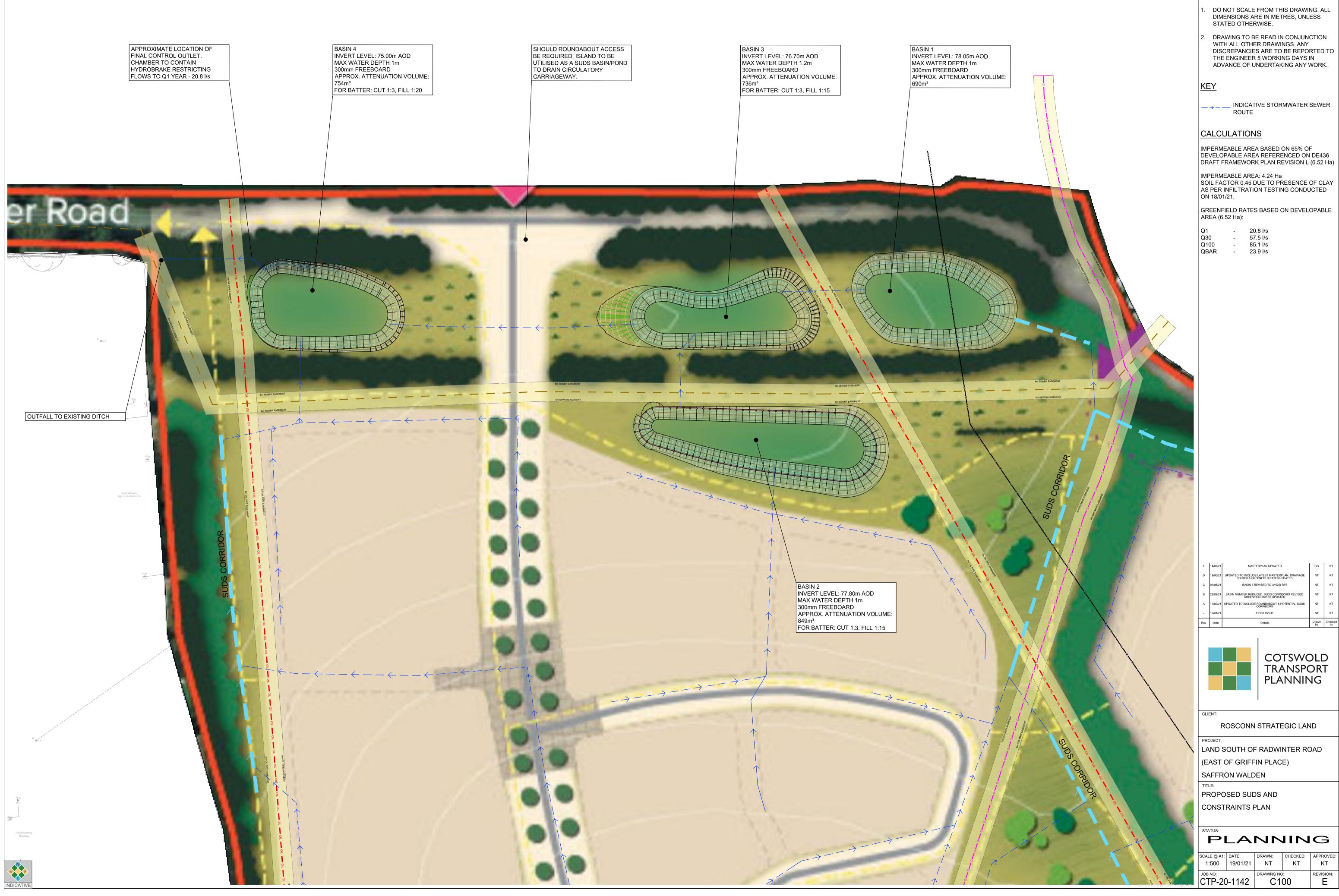
	Stor Even		Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)
360	min	Winter	14.061	0.0	3002.1	362
480	min	Winter	11.142	0.0	3171.8	476
600	min	Winter	9.297	0.0	3254.3	590
720	min	Winter	8.015	0.0	3291.7	704
960	min	Winter	6.338	0.0	3277.0	924
1440	min	Winter	4.546	0.0	3161.8	1296
2160	min	Winter	3.257	0.0	4172.1	1644
2880	min	Winter	2.568	0.0	4387.2	2112
4320	min	Winter	1.836	0.0	4704.5	2948
5760	min	Winter	1.445	0.0	4939.2	3696
7200	min	Winter	1.200	0.0	5127.0	4400
8640	min	Winter	1.031	0.0	5282.9	5016
10080	min	Winter	0.906	0.0	5418.7	5560

Cotswold Transport Planning	Page 3				
CTP House, Knapp Road	CTP-20-1142 Saffron Walden				
Cheltenham	Attenuation requirements				
Gloucestershire, GL50 3QQ	Up to 1 in 100 Year + 40% CC	Micro			
Date 19/06/2021 13:14	Designed by NT				
File 20-1142_QBAR AND ATTEN.SRCX	Checked by KT	Drainage			
Innovyze	Source Control 2020.1				
Rainfall Details Rainfall Model FSR Winter Storms Yes					
Return Period (years)	100 Cv (Summer) 0.750				
5 5	land and Wales Cv (Winter) 0.840 20.000 Shortest Storm (mins) 15				
	0.439 Longest Storm (mins) 10080				
Summer Storms	Yes Climate Change % +40				
<u>Time Area Diagram</u> Total Area (ha) 4.238					
Time (mins) Area Time (mins	s) Area Time (mins) Area Time (mins) Area				
From: To: (ha) From: To:	(ha) From: To: (ha) From: To: (ha)				
0 4 1.059 4	8 1.060 8 12 1.059 12 16 1.060)			

Cotswold Transport Planning	P	age 4		
CTP House, Knapp Road	CTP-20-1142 Saffron Walden			
Cheltenham	Attenuation requirements			
Gloucestershire, GL50 3QQ	Up to 1 in 100 Year + 40% CC			
Date 19/06/2021 13:14	Designed by NT	Micro		
File 20-1142 QBAR AND ATTEN.SRCX	Checked by KT	Drainage		
Innovyze	Source Control 2020.1			
	Source control 2020.1			
	Model Details			
Storage i	s Online Cover Level (m) 79.000			
<u>Ta</u>	ank or Pond Structure			
	Invert Level (m) 78.000			
Depth (m)) Area (m²) Depth (m) Area (m²)			
0.000	0 2450.0 1.000 3004.7			
<u>Hydro-Bra</u>	ake® Optimum Outflow Control			
	Unit Reference MD-SHE-0201-2080-1100-2080			
	Design Head (m) 1.100 Sign Flow (1/s) 20.8			
Des	Flush-Flo™ Calculated			
	Objective Minimise upstream storage			
	Application Surface			
	Sump AvailableYesDiameter (mm)201			
Ir	nvert Level (m) 77.900			
Minimum Outlet Pipe				
Suggested Manhole	e Diameter (mm) 1500			
Control Points Head (m)	Flow (1/s) Control Points Head (m) Flow	(1/s)		
Design Point (Calculated) 1.100	20.8 Kick-Flo® 0.777	17.6		
Flush-Flo™ 0.360	20.8 Mean Flow over Head Range -	17.6		
1 2 5	pased on the Head/Discharge relationship for the Hyd			
Optimum as specified. Should another type of control device other than a Hydro-Brake Optimum® be utilised then these storage routing calculations will be invalidated				
Depth (m) Flow (1/s) Depth (m) Flow (1/s)	Depth (m) Flow (1/s) Depth (m) Flow (1/s) Depth (m	n) Flow (l/s)		
0.100 6.9 0.800 17.9	2.000 27.7 4.000 38.6 7.00	50.6		
0.200 19.0 1.000 19.9				
0.300 20.7 1.200 21.7				
0.400 20.7 1.400 23.3				
0.500 20.4 1.600 24.9 0.600 20.0 1.800 26.3				

Appendix G

Drainage Strategy



NOTES:

- DO NOT SCALE FROM THIS DRAWING. ALL DIMENSIONS ARE IN METRES, UNLESS STATED OTHERWISE.
- DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS. ANY DISCREPANCIES ARE TO BE REPORTED TO THE ENGINEER 5 WORKING DAYS IN ADVANCE OF UNDERTAKING ANY WORK.

KEY

_ INDICATIVE STORMWATER SEWER $\rightarrow - -$ ROUTE

CALCULATIONS

IMPERMEABLE AREA BASED ON 65% OF DEVELOPABLE AREA REFERENCED ON DE436 DRAFT FRAMEWORK PLAN REVISION L (6.52 Ha)

IMPERMEABLE AREA: 4.24 Ha SOIL FACTOR 0.45 DUE TO PRESENCE OF CLAY AS PER INFILTRATION TESTING CONDUCTED ON 18/01/21.

GREENFIELD RATES BASED ON DEVELOPABLE AREA (6.52 Ha):

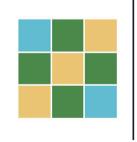
Q1 Q30 Q100 QBAR	-	20.8 l/s
Q30	-	57.5 l/s
Q100	-	85.1 l/s
QBAR	-	23.9 l/s

Е	14/07/21	MASTERPLAN UPDATED	CG	кт
D	19/06/21	UPDATED TO INCLUDE LATEST MASTERPLAN. DRAINAGE ROUTES & GREENFIELD RATES UPDATED	NT	кт
С	01/06/21	BASIN 3 REVISED TO AVOID RPZ	NT	кт
в	22/02/21	BASIN NUMBER REDUCED. SUDS CORRIDORS REVISED. GREENFIELD RATES UPDATED	NT	кт
А	17/02/21	UPDATED TO INCLUDE ROUNDABOUT & POTENTIAL SUDS CORRIDORS	NT	кт
-	19/01/21	FIRST ISSUE	NT	кт
Rev	Date	Details	Drawn by	Checke by

ROSCONN STRATEGIC LAND

PLANNING

REVISION: Е



PROJECT:

TITLE:

STATUS:

COTSWOLD TRANSPORT PLANNING



20m	NOTES: 1. DO NOT SCALE FROM THIS DRAWING. ALL DIMENSIONS ARE IN METRES, UNLESS STATED OTHERWISE.
	2. DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS. ANY DISCREPANCIES ARE TO BE REPORTED TO THE ENGINEER 5 WORKING DAYS IN ADVANCE OF UNDERTAKING ANY WORK.
	<u>KEY</u>
	\longrightarrow — \rightarrow — INDICATIVE STORMWATER SEWER ROUTE
	CALCULATIONS
LONG SECTION AMS AT 20m)	IMPERMEABLE AREA BASED ON 65% OF
I.T.S	DEVELOPABLE AREA REFERENCED ON DE436 DRAFT FRAMEWORK PLAN REVISION L (6.52Ha)
	IMPERMEABLE AREA: 4.28 Ha SOIL FACTOR 0.45 DUE TO PRESENCE OF CLAY AS PER INFILTRATION TESTING CONDUCTED ON 18/01/21.
	GREENFIELD RATES:
	Q1 - 20.8 l/s Q30 - 57.5 l/s Q100 - 85.1 l/s QBAR - 23.9 l/s
SWALE CROSS SECTION SCALE: N.T.S	
	B 140721 MASTERPLAN UPDATED CG KT A 199021 BASIN NUMBER REDUCED, SUGS CORRIDORS AMENDED. NT KT 1 800221 FIRST ISSUE NT KT 1 800221 FIRST ISSUE NT KT 1 800221 FIRST ISSUE Draw Organ Organ 1 800221 FIRST ISSUE T KT KT 1 800221 FIRST ISSUE Draw Organ Organ 1 800221 FIRST ISSUE Draw Draw Organ Organ 1 800221 Deala Draw Draw Organ Organ Organ 1 800221 Deala Draw Draw Draw Organ Organ 1 800221 Deala Draw Draw Draw Organ Organ 1 800221 Deala Draw Draw Draw Draw Organ 1 80021 Deala Draw Draw Draw Draw Draw Draw CLIENT: ROSCONN STRATEGIC LAND HT T R Draw D
	(EAST OF GRIFFIN PLACE) SAFFRON WALDEN
	DRAINAGE CONCEPT & SUDS PLAN
	STATUS: PLANNING
	SCALE @ A1: DATE: DRAWN: CHECKED: APPROVED: 1:1000 18/02/21 NT KT KT
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Appendix H

SuDs Water Quantity & Quality - LLFA Technical Appendix Proforma



Introduction

This proforma identifies the information required by Essex LLFA to enable technical assessment the Designers approach to water quantity and water quality as part of SuDS design approach in compliance with Essex SuDS Design Guide.

Completion of the proforma will also allow for technical assessment against Non-statutory technical standards (NSTS) for Sustainable Drainage. The proforma will accompany the site specific Flood Risk Assessment and Drainage Strategy submitted as part of the planning application.

Please complete this form in full for full applications and the coloured sections for outline applications. This will help us identify what information has been included and will assist with a smoother and quicker application.

Instructions for use

Use the units defined for input of figures Numbers in brackets refer to accompanying notes.

Where $\dots m^3$ $\dots m^3/m^2$ are noted – both values should be filled in.

Site details

- 1.1 Planning application reference (if known)
- 1.2 Site name
- 1.3 Total application site area ⁽¹⁾
 - 1.4 Predevelopment use ⁽⁴⁾
 - 1.5 Post development use If other, please sepcify
 - 1.6 Urban creep applicable
 - 1.7 Proposed design life / planning application life
 - 1.8 Method(s) of discharge: (5)

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Reuse Ir
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Infiltration

Waterbody

if yes, factor applied:

ha

Storm sewer

Combined sewer

- 1.9 Is discharge <u>direct</u> to estuary / sea
- 1.10 Have agreements in principle (where applicable) for discharge been provided

Hybrid



Calculation inputs

- Area within site which is drained by SuDS ⁽²⁾ m² 2.1 m²
- Impermeable area drained pre development ⁽³⁾ 2.2
- Impermeable area drained post development (3) m² 2.3
- 2.4 Additional impermeable area (2.3 minus 2.2)
- 2.5 Method for assessing greenfield runoff rate
- 2.6 Method for assessing brownfield runoff rate
- Coefficient of runoff (Cv) (6) 2.7
- 2.8 Source of rainfall data (FEH Preferred)
- 2.9 Climate change factor applied

Attenuation (positive outlet)

Drainage outlet at risk of drowning (tidal locking, elevated water levels in watercourse/sewer) 2.10 Note: Vortex controls require conditions of free discharge to operate as per manufacturers specification.

%

m²

2.11	Invert level at final outlet	mAOD				
2.12	Design level used for surcharge water level	at point of dischar	ge ⁽¹⁶⁾	mAOD		
Infiltratio	Infiltration (Discharge to Ground)					
2.13	Have infiltration tests been undertaken					
2.14	If yes, which method has been used					
2.15	Infiltration rate (where applicable)		m/s			
2.16	Depth to highest known ground water table	•	mAOD			
2.17	If there are multiple infiltration features plea	se specify where	they can be found in	the FRA		
2.18	Depth of infiltration feature		mAOD			
2.19	Factor of safety used for sizing infiltration s	torage				



Calculation outputs Sections 3 and 4 refer to site where storage is provided by full attenuation or partial infiltration. Where all flows are infiltrated to ground go straight to Section 6.

3 .0	Greenfield runoff rates (incl. Urban Creep)					
3.1	1 in 1 year rainfall	l/s/ha,		I/s for the site		
3.2	1 in 30 year rainfall	l/s/ha,		I/s for the site		
3.3	1 in 100 year rainfall + CCA	l/s/ha,		I/s for the site		
4.0	Brownfield runoff rates (incl. Urban Cr	eep)				
4.1	1 in 1 year rainfall	l/s/ha,		I/s for the site		
4.2	1 in 30 year rainfall	l/s/ha,		I/s for the site		
4.3	1 in 100 year rainfall + CCA	l/s/ha,		I/s for the site		
5.0	Proposed maximum rate of runoff from	n site (incl. Ur	ban Cr	ee p) ⁽⁷⁾		
5.1	1 in 1 year rainfall	l/s/ha,		I/s for the site		
5.2	1 in 30 year rainfall	l/s/ha,		I/s for the site		
5.3	1 in 100 year rainfall + CCA	l/s/ha,		I/s for the site		
6 .0	Attenuation storage to manage flow rate	s from site (ind	cl. Clima	ate Change Allowance (CCA) and Urban Creep)		
6.1	Storage - 1 in 100 year + CCA ⁽⁹⁾		m ³	m ³ /m ²		
6.2	50% storage drain down time 1 in 30 yea	rs		hours		
7.0	Controlling volume of runoff from the site ^{(*}	10)				
7.1	Pre development runoff volume ⁽¹²⁾ (development area)			m ³ for the site		
7.2	Post development runoff volume (unmitigated) ⁽¹²⁾			m ³ for the site		
7.3	Volume to be controlled (5.2 - 5.1)			m ³ for the site		



	Volume control provided by: Interception losses ⁽¹³⁾ Rain harvesting ⁽¹⁴⁾	m ³ m ³				
-		m ³ m ³				
	Attenuation			3		
-	Separate volume designated as long to		m ³			
7.5	5 Total volume control (sum of inputs for 5.4)			m ³ (17)		
8.0 S	8.0 Site storage volumes (full infiltration only)					
8.1	Storage - 1in 30 year + CCA ⁽⁸⁾		m ³	m^3/m^2 (of developed impermeable area)		
8.2	Storage - 1 in 100 year + CCA (11)		m ³	m ³ / m ²		

Design Inputs

Proposed site use

Pollution hazard category (see C753 Table 26.2)

High risk area defined as area storing fuels chemicals, refuelling area, washdown area, loading bay.

Design Outputs

List order of SuDS techniques proposed for treatment

Note that gully pots, pipes and tanks are not accepted by Essex LLFA as a form of treatment (for justification see C753 Section 4.1, Table 26.15 and Box B.2)

Are very high pollution risk areas drained separate from SuDS to foul system

Other

Please include any other information that is relevant to your application



Notes

- 1. All area with the proposed application site boundary to be included.
- The site area which is positively drained includes all green areas which drain to the SuDS system and area of surface SuDS features. It excludes large open green spaces which do not drain to the SuDS system.
- 3. Impermeable area should be measured pre and post development. Impermeable surfaces include, roofs, pavements, driveways and paths where runoff is conveyed to the drainage system.
- 4. Predevelopment use may impact on the allowable discharge rate. The LLFA will seek for reduction in flow rates to GF (Essex SuDS Design Guide).
- 5. Runoff may be discharge via one or more methods.
- 6. Sewers for Adoption 6th Edition recommends a Cv of 100% when designing drainage for impermeable area (assumes no loss of runoff from impermeable surfaces) and 0% for permeable areas. Where lower Cv's are used the applicant should justify the selection of Cv.
- 7. It is Essex County Council's preference that discharge rates for all events up to the 1 in 100 year event plus climate change are limited to the 1 in 1 greenfield rate. This is also considered to mitigate the increased runoff volumes that occur with the introduction of impermeable surfaces. If discharge rates are limited to a range of matched greenfield flows then it is necessary to provide additional mitigation of increased runoff volumes by the provision of Long-term Storage.
- 8. Storage for the 1 in 30 year must be fully contained within the SuDS components. Note that standing water within SuDS components such as ponds, basins and swales is not classified as flooding. Storage should be calculated for the critical duration rainfall event.
- 9. Runoff generated from rainfall events up to the 1 in 100 year will not be allowed to leave the site in an uncontrolled way. Temporary flooding of designated areas to shallow depths and velocities may be acceptable.
- 10. The following information should only be provided if increased runoff volumes are not mitigated by limiting all discharge rates back to the greenfield 1 in 1 year rate.
- 11. Climate change is specified as 40% increase to rainfall intensity, unless otherwise agreed with the LLFA / EA.
- 12. To be determined using the 100 year return period 6 hour duration winter rainfall event.
- 13. Where Source Control is provided Interception losses will occur. An allowance of <u>5mm rainfall</u> <u>depth</u> can be subtracted from the net inflow to the storage calculation where interception losses are demonstrated. The Applicant should demonstrate use of subcatchments and source control techniques. Further information is available in the SuDS Design Guide.
- 14. Please refer to Rain harvesting BS for guidance on available storage.
- 15. Flows within long term storage areas should be infiltrated to the ground or discharged at low flow rate of maximum 2 l/s/ha.
- 16. Careful consideration should be used for calculations where flow control / storage is likely to be influenced by surcharged sewer or peak levels within a watercourse. Outlets can be tidally locked where discharge is direct to estuary or sea. Calculations should demonstrate that risk of downed outlet has been taken into consideration. Vortex controls require conditions of free discharge to operate as per specification.
- 17. In controlling the volume of runoff the total volume from mitigation measures should be greater than or equal to the additional volume generated.